

# Supplement

## Figures

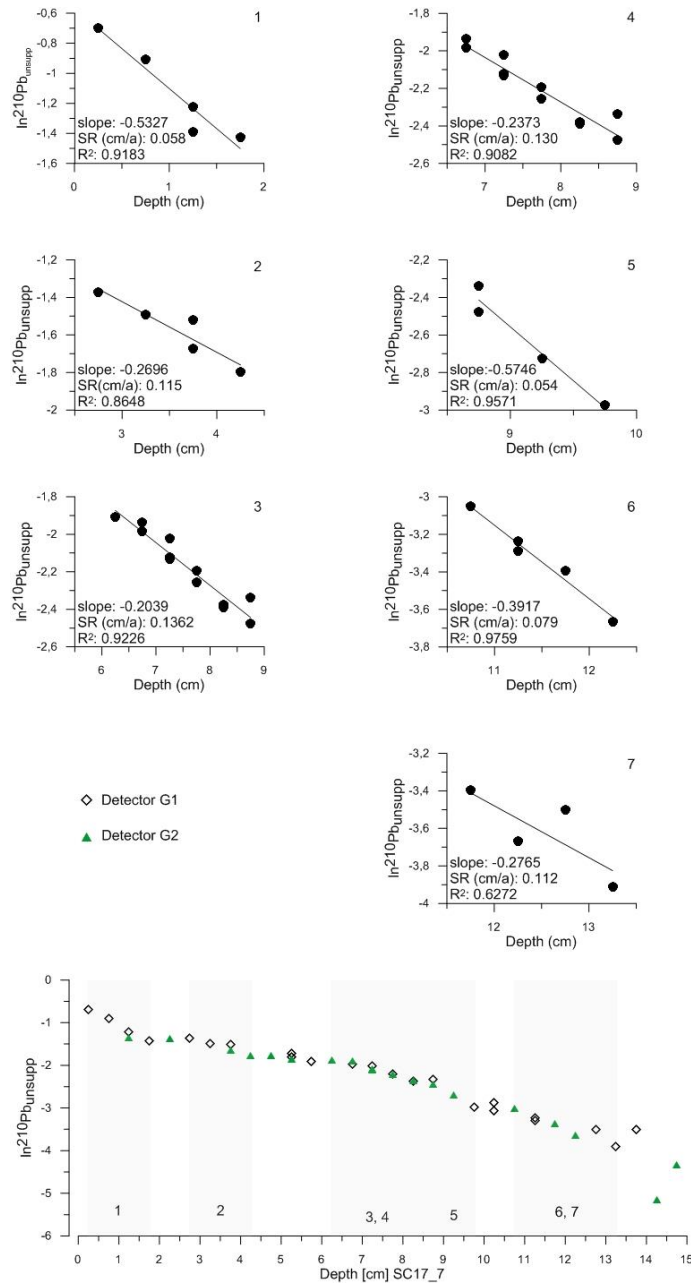


Suppl. Fig. 1 Correlation of SC17\_7 (right) with the top of the composite profile CHAT12 (left): Red lines signify marker layers. Dotted red lines indicate slightly calcitic enriched intervals. Thin sections are displayed next to the composite.

Suppl. Tab. 1 Gamma spectrometry results. count unc. = count uncertainty, \* not used for CRS model calculations.

		keV		661.66		46.54		295.24		351.93							
		Abundance		0.851		0.0425		0.185		0.358							
		Efficiency G1		0.163		0.6056		0.3626		0.3217							
		Efficiency G2		0.176		0.6638		0.3942		0.3319							
Composite	Depth	DD	m	Det	t <sub>mess</sub>	<sup>137</sup> Cs	<sup>137</sup> Cs	<sup>210</sup> Pb	<sup>210</sup> Pb	<sup>214</sup> Pb	<sup>214</sup> Pb	<sup>214</sup> Pb	<sup>214</sup> Pb	<sup>210</sup> Pb <sub>supp</sub>	<sup>210</sup> Pb <sub>unsupp</sub>	Sample	
Depth	(cm)	(g/cm <sup>3</sup> )	(g)		(d)	(mBq/g)	count	(mBq/g)	count	(mBq/g)	count	(mBq/g)	count	(mBq/g)	(mBq/g)	Number	
(cm)	Core						unc.		unc.		unc.		unc.(%)				
17-7	SC						(%)		(%)		(%)						
-1.0	0.25	0.164	1.04366	G1	3.06	53.6	2.6	512.4	2.2	12.2	11.0	15.5	5.5	13.9	498.6	1	
-0.5	0.75	0.294	1.12885	G1	3.79	49.3	2.2	424.1	2.1	22.5	5.9	18.8	2.5	20.6	403.5	2	
0.0	1.25	0.319	1.06359	G2	3.06	47.3	2.9	264.4	3.4	16.8	8.3	13.0	6.0	14.9	249.5*	3	
0.0	1.25	0.319	1.06359	G1	6.99	48.4	1.8	308.1	2.1	13.2	6.0	13.4	4.2	13.3	294.8	4	
0.5	1.75	0.207	1.02092	G1	2.70	65.1	2.5	259.7	3.5	20.5	7.8	19.5	5.3	20.0	239.7	5	
1.0	2.25	0.156	1.08748	G2	3.17	97.6	1.7	266.2	3.1	25.9	5.9	17.8	5.1	21.8	244.4	6	
1.5	2.75	0.138	1.02426	G1	3.85	162.1	1.2	279.6	3.0	25.0	7.8	26.9	4.5	26.0	253.6	7	
2.0	3.25	0.135	1.02441	G1	3.14	209.0	1.2	253.4	3.7	27.2	7.4	30.3	4.2	28.7	224.7	8	
2.5	3.75	0.147	1.14065	G1	1.98	236.1	1.3	251.8	4.6	34.5	6.9	32.1	4.8	33.3	218.5*	9	
2.5	3.75	0.147	1.14065	G2	5.02	236.3	0.8	217.3	2.8	28.8	5.3	30.9	3.3	29.8	187.5	10	
3.0	4.25	0.144	1.18116	G2	2.00	266.4	1.2	195.5	5.4	32.2	7.4	26.7	6.1	29.5	166.0	11	
3.5	4.75	0.107	1.06028	G2	4.89	302.7	0.7	196.8	3.6	30.6	51.7	33.1	4.0	31.9	165.0	12	
4.0	5.25	0.112	1.00751	G1	3.16	295.8	1.0	202.8	4.5	40.5	5.3	36.3	3.7	38.4	164.4*	13	
4.0	5.25	0.112	1.00751	G1	4.18	296.3	0.9	215.6	3.5	40.4	4.5	34.6	3.2	37.5	178.1*	14	
4.0	5.25	0.112	1.00751	G2	6.73	300.3	0.7	185.5	4.3	33.7	4.7	35.3	3.1	34.5	151.0	15	
4.5	5.75	0.132	1.08969	G1	2.94	259.5	1.1	182.8	5.0	32.0	6.4	36.6	3.7	34.3	148.5	16	
5.0	6.25	0.146	1.04027	G2	3.17	202.3	1.2	187.6	4.4	36.0	5.9	41.8	3.8	38.9	148.7	17	
5.5	6.75	0.137	1.0732	G1	2.98	133.1	1.5	174.8	4.6	38.4	5.5	35.9	3.6	37.1	137.7*	18	
5.5	6.75	0.137	1.0732	G2	4.20	136.7	1.2	180.7	5.0	37.0	5.5	35.4	3.5	36.2	144.5	19	
6.0	7.25	0.169	0.98522	G1	1.84	93.2	2.5	171.7	6.4	46.8	6.5	32.3	5.2	39.6	132.1*	20	
6.0	7.25	0.169	0.98522	G2	3.85	95.8	1.7	154.6	5.1	32.6	6.8	39.7	3.5	36.1	118.5*	21	
6.0	7.25	0.169	0.98522	G2	6.99	94.8	1.3	161.8	4.6	41.2	3.9	43.2	2.4	42.2	119.6	22	
6.5	7.75	0.140	1.04013	G2	2.95	65.8	2.4	145.7	6.2	41.3	4.9	40.4	3.3	40.9	104.9*	23	
6.5	7.75	0.140	1.04013	G1	4.90	62.3	1.9	151.7	4.4	42.4	3.8	37.8	2.8	40.1	111.6	24	
7.0	8.25	0.132	0.97056	G2	2.97	51.8	2.9	134.0	7.1	45.7	5.5	39.1	3.8	42.4	91.6*	25	
7.0	8.25	0.132	0.97056	G1	3.15	48.9	2.7	135.1	5.6	45.8	4.8	38.8	3.5	42.3	92.8	26	

Composite Depth (cm)	Depth (cm) Core SC 17-7	DD (g/cm <sup>3</sup> )	m (g)	Det	t <sub>mess</sub> (d)	<sup>137</sup> Cs (mBq/g)	<sup>137</sup> Cs count unc. (%)	<sup>210</sup> Pb (mBq/g)	<sup>210</sup> Pb count unc. (%)	<sup>214</sup> Pb (mBq/g)	<sup>214</sup> Pb count unc. (%)	<sup>214</sup> Pb (mBq/g)	<sup>214</sup> Pb count unc.(%)	<sup>210</sup> Pb <sub>supp</sub> (mBq/g)	<sup>210</sup> Pb <sub>unsupp</sub> (mBq/g)	Sample Number
7.5	8.75	0.168	1.13756	G2	2.71	41.7	2.9	124.6	5.7	38.9	6.0	41.9	3.5	40.4	84.2*	27
7.5	8.75	0.168	1.13756	G1	2.91	38.9	3.0	134.6	6.2	39.1	4.9	37.2	3.3	38.1	96.5	28
8.0	9.25	0.148	1.15022	G2	2.99	26.6	3.7	89.1	8.0	36.9	5.2	40.4	3.1	38.6	65.5	29
8.5	9.75	0.116	1.07792	G1	2.16	16.9	6.4	95.0	10.0	46.1	5.4	41.8	4.0	43.9	51.5	30
9.0	10.25	0.138	1.04675	G1	4.08	12.5	6.2	97.0	8.6	44.6	4.6	37.4	3.3	41.0	56.1*	31
9.0	10.25	0.138	1.04675	G1	6.73	14.3	4.8	88.4	6.0	42.1	3.6	40.8	2.7	41.5	46.9	32
9.5	10.75	0.106	1.06813	G2	2.16	10.8	8.1	84.3	9.9	34.9	7.1	39.2	3.9	37.1	47.2	33
10.0	11.25	0.131	0.9888	G1	3.98	9.7	9.1	79.9	7.9	43.1	7.9	38.2	3.4	40.7	39.3	34
10.0	11.25	0.131	0.9888	G1	3.81	7.1	12.0	75.5	8.1	37.2	8.1	39.2	3.0	38.2	37.3*	35
10.5	11.75	0.156	1.18173	G2	2.91	7.0	11.2	72.0	8.4	39.0	8.4	38.0	3.4	38.5	33.5	36
11.0	12.25	0.168	1.08336	G2	4.09	4.2	15.7	63.8	8.0	36.7	8.0	39.8	3.1	38.2	25.6	37
11.5	12.75	0.146	1.14027	G1	3.95	4.5	14.6	68.4	9.0	38.9	9.0	37.5	2.9	38.2	30.2	38
12.0	13.25	0.183	0.95955	G1	2.88	3.7	26.9	64.0	11.0	46.8	11.0	41.1	4.0	44.0	20.0	39
12.5	13.75	0.154	1.28248	G1	3.78	3.7	16.4	69.2	9.6	39.5	9.6	39.3	2.7	39.4	29.7	40
13.0	14.25	0.154	0.98268	G2	7.93	3.2	17.9	49.6	7.7	41.7	7.7	46.4	2.1	44.1	5.5	41
13.5	14.75	0.112	1.09286	G2	2.99	3.3	16.5	51.9	11.9	40.8	11.9	37.7	3.4	39.3	12.6	42



Suppl. Fig. 2  $\ln^{210}\text{Pb}_{\text{unsupp}}$  vs depth plot and depth sequences used to calculate sedimentation rates for the CIC model. Light grey bars indicate the used sequences. White square= Detector G1, green triangles= Detector G2.

Suppl. Tab. 2 Age determination by used depth sequences of  $\ln^{210}\text{Pb}_{\text{unSUPP}}$ . The CIC model assumes equal initial concentrations of  $^{210}\text{Pb}_{\text{unSUPP}}$  in the sediment regardless of the mass flux at the coring site (c.f. Appleby, 2002). Intercalated sediment sections showed nearly uncorrelated  $\ln(^{210}\text{Pb}_{\text{unSUPP}})$  vs. depth relationships between 10.25-9.25, 6.25-4.25, 2.25-1.75 cm depth (Suppl. Fig. 2). Therefore, the initial  $^{210}\text{Pb}_{\text{unSUPP}}$  activities of samples that bridged these sections were additionally used to determine time intervals between these samples (italic sequences). We further constrained the CIC model to the  $^{137}\text{Cs}$  peak at 5.25 cm depth, located within an uncorrelated  $\ln(^{210}\text{Pb}_{\text{unSUPP}})$  vs. depth section between 6.25-4.25 cm depth, assuming it represents the AD 1963 peak of atmospheric nuclear weapon tests.

Marker/ Depth (cm)	Age Marker	Seq. No.	from	to	delta _x (cm)	slope	SR (cm/a)	delta t (a)	R <sup>2</sup>	Dated depths in SC17_7	Comment
0.25	2015										Assumed rel. to top = 2017
1.75	-	1	0.25	1.75	1,5	-0.5327	0.0583	25.7	0.9183	1.75=1989.3	Calc rel to top (2015-25.7 a)
2.25	-	-	0.25	2.25	2	-	0,0872	22,9	-	2.25=1992,1	calc rel Top (2015-22,9)
5.25 – <sup>137</sup> Cs peak	1963 ?										Assuming that <sup>137</sup> Cs peak = AD 1963

2.25	-	-	2.25	4.25	2	-0.1943	0.1600	12.5	0.7793	2.25=1976.1	Cal rel to 4.25=1963.6
2.75	-	2	2.75	4.25	1.5	-0.2696	0.1153	13,0	0.8648	2.75=1976.6	Cal rel to 4.25=1963.6
2.75	-	-	2.75	4.25	1.5	-0,2094	0.107	14	0.9933	2.75=1977.6	Cal rel to 4.25=1963.6 (without Nr 9)
3.25	-	-	3.25	5.25	2	-	0,1989	10,1	-	3.25=1973,1	Cal rel to 4.25=1963.6
4.25	-	-	4.25	5.25	1	-0,0098	3.1717	0.6	0,978	4.25=1963.6	Cal rel to 5.25=1963, ~flat sequence
4.25	-	-	4.25	5.25	1	-	3.1647	0.3	-	4.25=1963.3	Cal rel to 5.25=1963, ~flat sequence
5.75	-	-	4.25	5.75	1.5	-0,0677	0.4591	3.3	0.6723	5.75=1960.3	without Nr 14 & 15
5.75	-	-	5.25	5.75	0.5	-	0.1527	3.3	-	5.75=1959,7	Cal rel to 5.25=1963
5.75	-	-	5.75	8.75	3	-02093	0.1485	20.2	0.9038	8.75=1939.5	Cal rel to 5.75=1959.7
6.25	-	-	5.25	6.25	2	-	0.6196	1.8	-	6.25= 1957.9	Cal rel to 5.75=1959.7
8.75	-	3	6.25	8.75	2.5	-0.2282	0.1362	18.4	0.9226	8.75= 1939.5	Cal rel to 6.25= 1957.9
8.25	-	-	5.75	8.25	3,0	-	0,1958	15.3	-	8.25=1944,4	Cal rel to 5.75=1959.7
8.75	-	-	5.25	8.75	3,5	-	0,1817	17,1	-	8.75=1945.9	Only 5.25 (G1; <sup>210</sup> Pb <sub>unSUPP</sub> =164.4 mBq/g) and 8,75 (G1)
8.75 – Onset <sup>137</sup> Cs increase	1945									8.75=1945.9	
7.25	-	-	7.25	8.75	1.5	-	0.1495	10	-	7.25=1955.9	Cal. rel. to 8.75=1945.9
9.75	-	5	8.75	9.75	1	-0,5746	0,0541	18.5	0,9571	9.75=1927.4	Slope change at 8.75, cal. rel. to 8.75=1945.9
10.75	-	-	8.75	10,75	2	-	0.0963	20.8	-	10.75=1925.1	~flat seq. between 9.75 and 10.25
11,75	-	-	8.75	11,75	3	-	0.0942	31,9	-	11.75 = 1914	~flat seq. between 9.75 and 10.25
12,25	-	6	10,75	12,25	1.5	-0,3917	0,0794	18,9	0,9759	12.25 = 1906.2	cal. rel. to 10.75=1925.1.
13,25	-	7	11.75	13.25	1.5	-0,2765	0,1124	13,3	0,6272	13.25=1900.7	cal. rel. to 11.75=1914
13.25	-	-	12.25	13.25	1	-	0,1267	7,9	-	13.25 = 1898.3	cal. rel. to 12.25=1906.2
13.75	-	-	12,25	13.75	-	-	0,3093	4,8	-	13.75=1901.4	cal. rel.to 12.25=1906.2
14.75	-	-	12.25	14.75	2.5	-	0,1103	22,7	-	14.75 = 1883.5	cal. rel.to 12.25=1906.2

Supp. Tab. 3) Comparison of CIC and CRS model chronologies, calculated sedimentation rates (cm/a) and mass acc. rates (g/cm<sup>2</sup>/a). Data based on Suppl. Tab. 1 & 2.

Depth SC17_7 (cm)	Composite depth (cm)	*CIC- Model Age	SR (cm/a) CIC Model	*CRS-Model age	SR (cm/a) CRS Model	mass acc. rate (g/cm <sup>2</sup> /a)
0.25	-1.0	2015	0.06	2015	0.14	0.022
0.75	-0.5	-	0.06	2010	0.08	0.024
1.25	0.0	-	0.06	2004	0.09	0.027
1.75	0.5	1989.3	0.06	1999	0.13	0.027
2.25	1.0	1976.1	0.16	1996	0.15	0.024
2.75	1.5	1976.6	0.12	1993	0.15	0.020
3.25	2.0	1973.1	0.12	1989	0.15	0.021
3.75	2.5	-	0.12	1986	0.15	0.022
4.25	3.0	-	0.12	1983	0.16	0.023
4.75	3.5	-	-	1980	0.19	0.020
5.25	4.0	1963	-	1977	0.18	0.021
5.75	4.5	1959.7	0.15	1974	0.15	0.019
6.25	5.0	-	0.15	1970	0.12	0.017
6.75	5.5	1961.2	0.13	1966	0.11	0.015
7.25	6.0	1955.9	0.13	1961	0.09	0.016
7.75	6.5	-	0.13	1956	0.10	0.014
8.25	7.0	-	0.13	1951	0.11	0.014
8.75	7.5	1945.9	0.13	1945	0.07	0.012
9.25	8.0	-	0.05	1939	0.09	0.013
9.75	8.5	1927.4	0.05	1934	0.12	0.014
10.25	9.0	-	-	1929	0.10	0.014
10.75	9.5	1925.1	0.08	1924	0.11	0.011
11.25	10.0	-	0.08	1919	0.09	0.012
11.75	10.5	1914	0.08	1913	0.07	0.011
12.25	11.0	1906.2	0.08	1906	0.07	0.012
12.75	11.5	-	0.11	1898	0.05	0.008
13.25	12.0	1900.7	0.11	1887	0.04	0.008
13.75	12.5	-	-	1871	0.02	0.004
14.25	13.0	-	-	1854	0.04	0.006
14.75	13.5	1883.5	-	1832	0.02	0.002